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Plant name	Unit name	Boiler/NOx type	PM control	SOx control
Bruce Mansfield	-	CONV/PC/NOX/DRY	PARTSCRUB	NONE
Craig	СЗ	CONV/PC/NOX/DRY	BAGHOUSE	SDA
Craig (1984) And the second of	C1	CONV/PC/NOX/DRY	ESP- HS	WETSCRUB
Bailly	7	CYCLONE/NONOX/WET	ESP- CS	WETSCRUB
AES Hawaii, Inc.	A	FBC/SNCR	BAGHOUSE	FBC
Bay Front Plant Generating	ഗ	CYCLONE/NONOX/WET	MECH	COMP COAL
Presque Isle	6	CONV/PC/NONOX/WET	ESP- CS	COMP COAL
2	ڻ. ت	CONV/PC/NONOX/WET	ESP- CS	COMP COAL
200		CONV/PC/NOX/WET	ESP- HS	COMP COAL
	_	FBC/NONOX	BAGHOUSE	FBC
St Clair Power Plant		CONV/PC/NONOX/DRY	ESP- CS	COMP COAL
Control of the Contro	BB03	CONV/TURBO/NOX/WET	ESP- CS	WETSCRUB
and the state of t	ω	CONV/PC/NONOX/DRY	ESP- HS	WETSCRUB
The state of the s	-	CONV/PC/NOX/DRY	BAGHOUSE	COMP COAL
Intermountain Anna San San San San San San San San San	2SGA	CONV/PC/NOX/DRY	BAGHOUSE	WETSCRUB
Stockton Cogen Company	GEN1	FBC/SNCR	BAGHOUSE	FBC
Montrosé Company de Caracteria		CONV/PC/NOX/DRY	ESP- CS	COMP COAL
Rawhide	101	CONV/PC/NOX/DRY	BAGHOUSE	SDA
Valley	2	CONV/PC/NOX/DRY	BAGHOUSE	NONE
Shawnee Fossil Plant	ω	CONV/PC/NOX/DRY	BAGHOUSE	COMP COAL
Jim Bridger 1986 1986 1986 1986	BW 74	CONV/PC/NOX/DRY	ESP- CS	WETSCRUB
Laramie River Station	-	CONV/PC/NOX/DRY	ESP- CS	WETSCRUB
_aramie River Station	ω	CONV/PC/NOX/DRY	ESP- CS	SDA
_a Cygne	-	CYCLONE/NOX/WET	PARTSCRUB	WETSCRUB
Cliffside		CONV/PC/NONOX/DRY	ESP- HS	NONE
Sherburne County Generating Plant	#3	CONV/PC/NOX/DRY	BAGHOUSE	SDA
Meramec	4	CONV/PC/NOX/DRY	ESP- CS	NONE
Colstrip Transfer of the Colstrip Transfer of	ω	CONV/PC/NOX/DRY	PARTSCRUB	WETSCRUB
GRDA	2	CONV/PC/NOX/DRY	ESP- CS	SDA
Coronado	U1B	CONV/PC/NOX/WET	ESP- HS	WETSCRUB
Newton 2000 100 100 100 100 100 100 100 100 10	2	CONV/PC/NOX/DRY	ESP- CS	COMP COAL
Salem Harbor	ω	CONV/PC/NOX/SNCR/DRY	ESP- CS	COMP COAL
Columbia Andreas Columbia	_	CONV/PC/NOX/DRY	ESP- HS	COMP COAL
Cholla Service	ω	CONV/PC/NONOX/DRY	ESP- HS	NONE
Cholla Ch	N	CONV/PC/NONOX/DRY	MECH/PARTSCRUB	WETSCRUB
	The same of the sa	CONIV/DO/NIOVANET	בסם בס	

Plant name Wyodak Brayton Point Brayton Point Antelope Valley Station Lawrence Clay Boswell	Unit name BW 91 1 3 81 4	Boiler/NOx type CONV/PC/NOX/DRY CONV/PC/NOX/DRY CONV/PC/NOX/DRY CONV/PC/NOX/DRY CONV/PC/NOX/DRY CONV/PC/NOX/DRY CONV/PC/NOX/DRY CONV/PC/NOX/DRY	PM control ESP- CS ESP- CS ESP- CS BAGHOUSE PARTSCRUB BAGHOUSE PARTSCRUB	SOx control SDA COMP COAL COMP COAL SDA WETSCRUB COMP COAL WETSCRUB/COMP COAL WETSCRUB/COMP COAL
Leland Olds Station Dwayne Collier Battle Cogeneration Facility	2B	CYCLONE/NONOX/WET STOKER/NOX/DRY	ESP- CS	NONE SDA
Comanche	28	CONV/PC/NOX/DRY	BAGHOUSE	SDA COMP COAL
Gibson Generating Station (1990) Gibson Generating Station (1990)	ω	CONV/PC/NOX/DRY	ESP- CS	NONE
Wabash River Generating Station	1+1A	CONV/PC/NOX/DRY	ESP- CS	NONE
George Neal South	4	CONV/PC/NOX/DRY	ESP- CS	COMP COAL
Widows Crock Ecosi Plant		CYCLONE/NONOX/WET	ESP- HS	COMP COAL
Sam Saymour	6	CONV/PC/NONOX/DRY	ESP- CS	COMP COAL
Polk Power	<u>.</u> ω	CONV/PC/NONOX/DRY	ESP- CS	WETSCRUB
R.M. Heskett Station	B2 -	FBC/NONOX	COAL GAS	COAL GAS
Stanton Station	-	CONV/PC/NOX/DRY	ESP- CS	NONE
Charles B. Lowman	10	CONV/PC/NOX/DRY	BAGHOUSE	SDA
Dunkirk	0 N	CONV/PC/NONOX/DRY	ESP- HS	WETSCRUB
Jack Watson	4	CONV/PC/NOX/DRY	ESP- HS	COMP COAL
Moc Von Line Constitution of the Constitution	2	CONV/PC/NONOX/DRY	ESP- HS	WETSCRUB
Port Washington	GEN 1	CONV/PC/NOX/DRY	BAGHOUSE	SDA
Lewis & Clark	B. 4	CONV/PC/NONOX/DBV	ESP- CS	SORBENT INJ
Clover Power Station	2	CONV/PC/NOX/DRY	BAGHOUSE	NONE
W. H. Sammis	_	CONV/PC/NONOX/DRY	BAGHOUSE	NONE
Gaston		CONV/PC/NONOX/DRY	ESP- CS/BAGHOUSE	NONE
Coyote	_	CYCLONE/NONOX/WET	BAGHOUSE	SDA
LIIIESIOIEK	LIM1	CONV/PC/NOX/WET	ESP- CS	WETSCRUB

Scrubgrass Generating Company L. P. GEN1	AES Cayuga (NY) (formerly NYSEG Milliken) 2	R. D. Morrow Sr. Generating plant 2	3		Kline Township Cogen Facility GEN1	GEN 1	SEI - Birchwood Power Facility 1 C	Plant name Unit name
FBC/NONOX	CONV/PC/NOX/DRY	CONV/PC/NOX/DRY	CONV/PC/NONOX/DRY	CONV/PC/NONOX/DRY	FBC/NONOX	CONV/PC/NOX/SCR/DRY	CONV/PC/NOX/SCR/DRY	Boiler/NOx type
BAGHOUSE	ESP- CS	ESP- HS	ESP- CS	ESP- CS/BAGHOUSE	BAGHOUSE	BAGHOUSE	BAGHOUSE	PM control
FBC	WETSCRUB	WETSCRUB	WETSCRUB	NONE	FBC	SDA	SDA	SOx control

Bruce Mansfield Plant name			0.0608	SUBBITUMINOUS	Platte
Plant name	0.0429		0.0582	SUBBITUMINOUS	Chola
Plant name	0.0429		0.0582	SUBBITUMINOUS	Cholla
Amansfield			0.0575	SUBBITUMINOUS	Columbia
Plant name			0.0571	BITUMINOUS	Salem Harbor
Amansfield	0.0546		0.0570	BITUMINOUS	Newton
Plant name			0.0569	SUBBITUMINOUS	Coronado
Amansfield	0.0771		0.0557	SUBBITUMINOUS	GRDA
Plant name Petroleum Coke 0.0100 BITUMINOUS 0.0254 BITUMINOUS 0.0255 BITUMINOUS 0.0256 BITUMINOUS 0.0257 BITUMINOUS 0.0257 BITUMINOUS 0.0258 PETROLEUM COKE 0.0200 SUBBITUMINOUS 0.0250 SUBB			0.0555	SUBBITUMINOUS	Colstrip 3 - Color and a second a second and
Average Hg	0.0896		0.0539	SUBBITUMINOUS	Meramec Translation of the second of the sec
Average Hg			0.0528	SUBBITUMINOUS	Sherburne County Generating Plant
Amansfield Piant name Piant name Piant name Pettroleum Coke 0.0054 Bittuminous Mansfield Pettroleum Coke 0.0054 Bittuminous Mansfield Pettroleum Coke 0.0055 Bittuminous Mansfield Pettroleum Coke 0.0055 Bittuminous Mansfield Mansfiel			0.0523	BITUMINOUS	Cliffside
Average Hg	0.1249		0.0523	SUBBITUMINOUS	La Cygne Andrew State Communication
Average Hg			0.0521	SUBBITUMINOUS	Laramie River Station
Average Hg	1		0.0521	SUBBITUMINOUS	Laramie River Station
Average Hg	0.0480		0.0501	SUBBITUMINOUS	Jim Bridger
Average Hg	0.1064		0.0482	BITUMINOUS	Shawnee Fossil Plant
Average Hg			0.0475	_ 1	Valley 2007 2
Average Hg In tuel I			0.0469	SUBBITUMINOUS	Rawhide
Average Hg			0.0422	SUBBITUMINOUS	Montrose Control of the Control of t
Average Hg	0.0293		0.0404	BITUMINOUS	Stockton Cogen Company
Average Hg	0.0117		0.0391	BITUMINOUS	Intermountain ()
Average Hg			0.0388	BITUMINOUS	Valmont (1)
Amansfield Plant name PETROLEUM COKE 0.0100 BITUMINOUS 0.0254 BITUMINOUS BITUMINOUS PETROLEUM COKE 0.0254 BITUMINOUS Mansfield D.0254 BITUMINOUS BITUMINOUS D.0254 BITUMINOUS BITUMINOUS D.0254 BITUMINOUS BITUMINOUS BITUMINOUS D.0254 BITUMINOUS BITUMINOUS BITUMINOUS D.0254 BITUMINOUS BITUMINOUS D.0254 BITUMINOUS BITUMINOUS BITUMINOUS D.0254			0.0374	BITUMINOUS	Navajo
Average Hg	0.1035		0.0348	SUBBITUMINOUS	Big Bend
Average Hg In fuel I	0.0875		0.0344	SUBBITUMINOUS	St Clair Power Plant
Average Hg			0.0310	LIGNITE	TNP-One Community of the Community of th
Average Hg average Hg In fuel 2 (ppmw) name of fuel 2 (ppmw) name of fuel 2 (ppmw) Name of fuel 2 Name of fuel 2 <th< td=""><td>0.0508</td><td></td><td>0.0300</td><td>BITUMINOUS/PETROLEUM COKE</td><td>Presque Isle</td></th<>	0.0508		0.0300	BITUMINOUS/PETROLEUM COKE	Presque Isle
Plant name name of fuel 1 (ppmw) name of fuel 2 (pp mw) BITUMINOUS BITUMINOUS 0.0254 BITUMINOUS BITUMINOUS BITUMINOUS 0.0254 BITUMINOUS BITUMINOUS D.0254 <	0.0508		0.0300	BITUMINOUS/PETROLEUM COKE	Presque Isle
Average Hg average Hg average Hg in fuel 2 (ppmw) name of fuel 2 (ppmw) name of fuel 2 (ppmw) name of fuel 2 (ppmw) BITUMINOUS BITUMINOUS 0.0254 BITUMINOUS BITUMINOUS BITUMINOUS BITUMINOUS BITUMINOUS BITUMINOUS 0.0254 BITUMINOUS BITUMINOUS ITIRES TIRES TOM TOME TOM TOME TOM TOME AND TOME </td <td>0.0508</td> <td></td> <td>0.0300</td> <td>BITUMINOUS/PETROLEUM COKE</td> <td>Presque Isle</td>	0.0508		0.0300	BITUMINOUS/PETROLEUM COKE	Presque Isle
Average Hg in fuel in	0.0087		0.0289	BITUMINOUS	Bay Front Plant Generating
average Hg average Hg average Hg in fuel 2 (ppmw) name of fuel 2 (ppmw) name of fuel 2 (ppmw) BITUMINOUS BITUMINOUS (ppmw) BITUMINOUS BITUMINOUS PETROLEUM COKE 0.0254 BITUMINOUS BITUMINOUS BITUMINOUS BITUMINOUS In mame of fuel 2 ppmw) ppmw) PETROLEUM COKE 0.0254 BITUMINOUS PETROLEUM COKE PETROLEUM COKE </td <td>0.0211</td> <td></td> <td>0.0279</td> <td>SUBBITUMINOUS</td> <td>AES Hawaii, Inc.</td>	0.0211		0.0279	SUBBITUMINOUS	AES Hawaii, Inc.
average Hg average Hg in fuel 2 (pp mw) name of fuel 2 (pp Mansfield PETROLEUM COKE 0.0100 BITUMINOUS 0.0254 BITUMINOUS 0.0254 BITUMINOUS 0.0254 BITUMINOUS	0.0600		0.0254	BITUMINOUS - LOW SULFUR	Bailly
average Hg average Hg in fuel in fuel in fuel in fuel in fuel 2 (pp mansfield PETROLEUM COKE 0.0100 BITUMINOUS SUBBITUMINOUS 0.0254 BITUMINOUS	0.0367		0.0254	SUBBITUMINOUS	Craig La Caracter Control of Caracter Control
average Hg average Hg in fuel in fuel in fuel 2 (ppmw) name of fuel 2 (ppmw) name of fuel 2 (ppmw) PETROLEUM COKE 0.0100 BITUMINOUS	0.0367		0.0254	SUBBITUMINOUS	Craig * 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
average Hg in fuel name of fuel 1 (ppmw) name of fuel 2	0.1330	BITUMINOUS	0.0100	PETROLEUM COKE	Bruce Mansfield
	(ppmw)	name of fuel 2	(ppmw)	name of fuel 1	Plant name
	in fuel		in fuel		
	average Hg		average Hg		

		average Ho		average Hg
		in fuel		in fuel
Plant name	name of fuel 1	(ppmw)	name of fuel 2	(ppmw)
Wyodak	SUBBITUMINOUS	0.0633		
Brayton Point	BITUMINOUS	0.0654		
Brayton Point	BITUMINOUS	0.0654		
Antelope Valley Station	LIGNITE	0.0658		
Lawrence	SUBBITUMINOUS	0.0683	BITUMINOUS	0.0795
Clay Boswell	SUBBITUMINOUS	0.0701		
Clay Boswell	SUBBITUMINOUS	0.0701		
Clay Boswell (1988) (1988) (1988)	SUBBITUMINOUS	0.0701		
Cliffy Creek	SUBBITUMINOUS	0.0711	BITUMINOUS	0.1463
Leland Olds Station	LIGNITE	0.0717		
Dwayne Collier Battle Cogeneration Facility	BITUMINOUS	0.0767		
Comanche	SUBBITUMINOUS	0.0767		
Gibson Generating Station (0300)	BITUMINOUS	0.0772		
Gibson Generating Station (1099)	BITUMINOUS	0.0772		
Wabash River Generating Station	BITUMINOUS	0.0786	PETROLEUM COKE	0.0225
George Neal South	SUBBITUMINOUS	0.0800		
Nelson Dewey	SUBBITUMINOUS	0.0805		
Widows Creek Fossil Plant	BITUMINOUS	0.0846		
Sam Seymour	SUBBITUMINOUS	0.0852		
Polk Power () Policy Control (BITUMINOUS	0.0858	SUBBITUMINOUS	0.0360
R.M. Heskett Station	LIGNITE	0.0881		
Stanton Station	LIGNITE	0.0883		
Stanton Station	LIGNITE	0.0883		
Charles R. Lowman	BITUMINOUS	0.0900		
Dunkirk 17 10 10 10 10 10 10 10 10 10 10 10 10 10	BITUMINOUS	0.0902		
Jack Watson	BITUMINOUS	0.0918	SUBBITUMINOUS	0.1558
San Juan 1987 1987 1988 1988 1988 1988 1988 1988	SUBBITUMINOUS	0.0918		
Mecklenburg Cogeneration Facility	BITUMINOUS	0.0932		
Port Washington	BITUMINOUS	0.0954		
Lewis & Clark	LIGNITE	0.0967		
Clover Power Station	BITUMINOUS	0.0978		
W. H. Sammis	BITUMINOUS	0.1009		
Big Brown	LIGNITE	0.1319		
Gaston	BITUMINOUS	0.1342		ALL ALL AND THE PROPERTY OF TH
Coyote	LIGNITE	0.1348		
LIMESTONE STATE OF THE PROPERTY OF THE PROPERT	LIGNITE	0.1460		

	D	Senerating plant x			Kline Township Cogen Facility 1980 WASTE.		SEI - Birchwood Power Facility 1000 1000 1000 BITU	Plant name name	
WASTE BITUMINOUS	BITUMINOUS	BITUMINOUS	LIGNITE	LIGNITE	WASTE ANTHRACITE	BITUMINOUS	BITUMINOUS	name of fuel 1	æ
0.7029	0.3186	0.1958	0.1754	0.1754	0.1733	0.1727	0.1470	(ppmw)	average Hg in fuel
			SUBBITUMINOUS	SUBBITUMINOUS				name of fuel 2	
			0.0732	0.0732				(ppmw)	average Hg in fuel

					Hg out
		T control	CI in test coal	Hg in test coal	furnace/ Hg
Plant name	Fuel in test	inlet (C)	(ppm)	(ppm)	in coal
Bruce Mansfield	BITUMINOUS	141	767	0.0927	1.0925
Craig Was A Constitution of the Constitution o	SUBBITUMINOUS	139	117	0.0100	1.3182
Craig San Annual Craig	SUBBITUMINOUS	121	267	0.0227	
Bailly	BITUMINOUS	173	646	0.0700	
AES Hawaii, Inc.	SUBBITUMINOUS	137	46	0.0267	0.5510
Bay Front Plant Generating	BITUMINOUS	134	127	0.0600	2.0220
Presque Isle	BITUMINOUS/PETCOKE	153	197	0.0393	1.2009
Presque Isle	BITUMINOUS/PETCOKE	172	190	0.0429	1.4292
Presque se procedure proce	SUBBITUMINOUS	382	223	0.0682	0.9047
TNP-One Control of the Control of th	CONTE LIGNITE	181	133	0.2547	0.9477
	SUBBITUMINOUS/BITUMINOUS	140	333	0.0613	0.9373
Big Bend	BITUMINOUS	155	1767	0.1383	
Navajo	BITUMINOUS	155	150	0.0303	
Valmont	BITUMINOUS	147	39	0.0079	2.1637
Intermountain And And And And And And And And And An	BITUMINOUS	151	200	0.0233	
Stockton Cogen Company	BITUMINOUS/PETCOKE	148	583	0.0270	1.4795
Montrose Company of the Company of t	SUBBITUMINOUS	158	133	0.0997	0.1890
Rawhide	SUBBITUMINOUS	171	127	0.0733	1.9758
Valley Manager Control of the Contro	BITUMINOUS/PETCOKE	157	128	0.0124	1.8615
Shawnee Fossil Plant	BITUMINOUS/SUBBITUMINOUS	158	167	0.0283	1.5706
Jim Bridger	SUBBITUMINOUS	146	50	0.0733	
Laramie River Station	SUBBITUMINOUS	138	77	0.1193	
Laramie River Station	SUBBITUMINOUS	139	74	0.1247	0.5406
La Cygne	SUBBITUMINOUS	144	300	0.1033	
Cliffside	BITUMINOUS	342	1400	0.0600	1.9574
Sherburne County Generating Plant	SUBBITUMINOUS	147	102	0.0767	1.3605
Meramec (1) (1) (1) (2) (2) (2) (3)	SUBBITUMINOUS/BITUMINOUS	170	3620	0.0910	1.0291
Colstrip	SUBBITUMINOUS	139	67	0.0653	1.0864
GRDA	SUBBITUMINOUS/BITUMINOUS	156	399	0.1000	0.9573
Coronado	SUBBITUMINOUS	138	117	0.0350	
Newton	SUBBITUMINOUS	161	178	0.0707	1.3010
Salem Harbor	BITUMINOUS	126	100	0.0267	1.7010
Columbia	SUBBITUMINOUS	406	314	0.1000	1.6265
Cholla	SUBBITUMINOUS	359	50	0.0367	0.2595
Cholla	SUBBITUMINOUS	137	50	0.0400	0.7384
Platte Control of the	SUBBITUMINOUS	414	181	0.0900	1.7623

Limestone 162 50 0.13	LIGNITE 172 100	BITUMINOUS 336 333	Big Brown 185 133 0.28	W. H. Sammis 158 1233 0.10	Clove Power Station BITUMINOUS 139 520 0.15	LIGNITE 199 100	BITUMINOUS 406 1215	Cogeneration Facility BITUMINOUS 148 1893	SUBBITUMINOUS 143 167	son 150 761	BITUMINOUS 305 872	an 146 367 BITUMINOUS 146 367	176 28	LIGNITE 165 50	t Station 162 100	BITUMINOUS 171 1067	SUBBITUMINOUS 150 20	ossil Plant BITUMINOUS 160 333	SUBBITUMINOUS/PETCOKE 257 129	SUBBITUMINOUS 152 191	BITUMINOUS 176 600	BITUMINOUS 161 2100	nerating Station (0300) BITUMINOUS 156 1867	SUBBITUMINOUS 145 50	e Cogeneration Facility BITUMINOUS 168 1700	Station 202 91	SUBBITUMINOUS/BITUMINOUS 383 441	SUBBITUMINOUS 144 50	SUBBITUMINOUS 144 50	rell A STATE SUBBITUMINOUS 176 50	SUBBITUMINOUS 166 267	y Station 153 107	BITUMINOUS 122 967	oint BITUMINOUS 154 567		Plant name Fuel in test inlet (C) (ppm) (ppn	T control Cl in test coal Hg in test	
0.1390	0.1107	0.0593	0.2880	0.1060	0.1594	0.1193	0.0900	0.0967	0.0537	0.0537	0.1300	0.0803	0.0835	0.0823	0.0863	0.1000	0.1227	0.0247	0.0600	0.0900	0.0673	0.1390	0.1183	0.0922	0.0300	0.0405	0.0800	0.0660	0.0630	0.0567	0.0477	0.0620	0.0800	0.0633		(ppm)	oal Hg in test coal	
	1.4073	1.3715	0.7928	1.7640		1.4342	2.0011	1.2365		1.0654	1.1636		1.1531	0.5415	0.8195	0.6601		1.5506	0.4330	0.8520	0.6747	1.5660	3.1616	0.8542	0.7344	1.2793	1.8300	0.7233	1.0915	0.8920	1.0345	0.5942	1.1622	1.3004	4.1729	in coal	furnace/ Hg	Ha out

WASTE BITUMINOUS 161 600 0.5267	Plant name SEI - Birchwood Power Facility Logan Generating Plant Kline Township Cogen Facility Monticello Monticello R: D. Morrow Sr. Generating plant AES Cawara (NY) (formerly NYSEG Millicen)	Fuel in test BITUMINOUS BITUMINOUS WASTE BITUMINOUS LIGNITE LIGNITE BITUMINOUS	50	Cl in test coal (ppm) 917 1500 267 167 133 833 883	Hg in test coal (ppm) 0.1100 0.1800 0.3333 0.3717 0.4150 0.0500	Hg out furnace/ Hg in coal 0.9300 0.9117 0.2675 0.9671
LIGNITE 176 133 0.4150 BITUMINOUS 166 833 0.0500 Iken) BITUMINOUS 137 882 0.1065 WASTE BITUMINOUS 161 600 0.5267	Monticello	LIGNITE	181	167	0.3717	0.967
BITUMINOUS	Montticello 1995	LIGNITE	176	133	0.4150	
Iken) BITUMINOUS 137 882 0.1065 WASTE BITUMINOUS 161 600 0.5267	R. D. Morrow Sr. Generating plant	- 1	166	833	0.0500	
WASTE BITUMINOUS 161 600	AES Cayuga (NY) (formerly NYSEG Milliken)	BITUMINOUS	137	882	0.1065	
TO A DIVINE THE PROPERTY OF TH	Scrubgrass Generating Company L. P.	WASTE BITUMINOUS	161	600	0.5267	0.6937

0.8988 0.1195 -0.3627 -0.0435	0.8298 -0.2522 0.642 0.2436 -0.6753	no bypass no bypass no bypass no bypass no bypass	PM/ESP- CS PM/ESP- CS PM/ESP- HS PM/ESP- HS PM/ESP- HS	7.6144 3.2345 11.8709 0.9056 3.1632	8.3088 3.1869 13.3510 0.7940 2.6512	Newton Salem Harbor Columbia Cholla Cholla
0.744 -0.0784 -0.0283 -0.1524	0.7116 0.7472 -0.0097 0.3061	no bypass no bypass no bypass after control	PM/ESP- CS PM/PARTSCRUB SO2/WETSCRUB SO2/WETSCRUB	6.6269 6.1489 8.6306	6.8262 6.7042 7.8983	Sherburne County Generating Plant Meramec Colstrip GRDA Coronado
0.6074 -0.7848 0.2215 0.3041	0.1949 0.7338 0.7038 0.427 -0.1243	no bypass no bypass no bypass no bypass no bypass	SO2/WETSCRUB SO2/WETSCRUB SO2/SDA PM/PARTSCRUB PM/ESP- HS	6.2128 7.0920 6.4487	5.6025	Jim Bridger Laramie River Station Laramie River Station La Cygne Cliffside
0.9182 0.0933 0.3183 -0.0675 0.682	0.8927 0.3572 -0.2564 -1.086 0.4974	no bypass no bypass no bypass no bypass no bypass	PM/BAGHOUSE PM/ESP- CS SO2/SDA PM/BAGHOUSE PM/BAGHOUSE	1.7032 6.4935 11.6487 1.5799 3.3073	3.2006 1.7922 12.1599 1.6095 3.2737	Stockton Cogen Company Montrose Rawhide Valley Shawnee Fossil Plant
0.5698 0.2023 0.6852 0.2095 0.8652 0.7453	0.592 0.3649 0.8235 -0.2046 0.7733 0.8384	no bypass no bypass no bypass no bypass no bypass no bypass	PM/BAGHOUSE PM/BAGHOUSE PM/ESP- CS SO2/WETSCRUB SO2/WETSCRUB PM/BAGHOUSE SO2/WETSCRUB	4.8944 25.8212 4.8819 0.9228	5.1091 25.8893 4.5648 1.3706	Presque Isle TNP-One St Clair Power Plant Big Bend Navajo Valmont Intermountain
0.2819 0.4795 0.5252 -0.5707 0.5452 0.662	0.2367 0.5861 0.788 -0.4737 0.5802 0.6282 0.0993	no bypass no bypass no bypass no bypass no bypass no bypass	SO2/WETSCRUB SO2/WETSCRUB PM/BAGHOUSE PM/MECH PM/ESP- CS PM/ESP- CS	0.9854 2.3927 2.6811 3.7660	1.1256 9.5606 3.4866 4.7905	Craig Bailly AES Hawaii, Inc. Bay Front Plant Generating Presque Isle Presque Isle
fremove control 0.1207 0.336	fr.remove coal-stack 0.0799	location no bypass no bypass	tested control PM/PARTSCRUB SO2/SDA	F factor lb Hg/TBtu out furnace 8.0849 1.0972	lb Hg/TBtu out furnace 7.3950 1.0437	Plant name Bruce Mansfield Craig

0.3824	0.1211	no bypass	SO2/SDA	12.8692	13.5502	Coyote
-0.1719	-0.3998	no bypass	PM/ESP- HS	5.2148	5.9456	Gaston Control of the
-0.0808	0.1002	no bypass	PM/ESP- CS/BAGHOUSE	27.9212	25.8997	Big Brown
0.9221	0.8716	no bypass	PM/BAGHOUSE	10.7427	14.0602	W. H. Sammis
0.7633	0.9671	no bypass	SO2/WETSCRUB			Clover Power Station
0.3277	0.1995	no bypass	PM/PARTSCRUB	16.9607	16.1501	-ewis & Clark
0.4489	0.0118	no bypass	SO2/SORBENT INJ	12.2227	12.8800	Port Washington
0.9881	0.9851	no bypass	SO2/SDA	9.9299	8.3530	Mecklenburg Cogeneration Facility
0.3683	0.1747	after control	SO2/WETSCRUB			San Juan
0.2923	0.2447	no bypass	PM/ESP- CS	4.1634	4.3276	Jack Watson
0.1873	0.1019	no bypass	PM/ESP- HS	8.3305	10.8768	Dunkirk Andrews Communication of the Communication
0.7324	0.8397	after bypass	SO2/WETSCRUB			Charles R. Lowman
0.0147	-0.0701	no bypass	SO2/SDA	6.3462	8.7844	Stanton Station Control of the Contr
-0.0357	0.4409	no bypass	PM/ESP- CS	6.6754	3.2952	Stanton Station Station
0.4036	0.5614	no bypass	PM/ESP- CS	7.3244	6.5466	R.M. Heskett Station
0	0.3399	no bypass	no control	5.4713	5.2289	Polk Power
-0.2032	0.5624	after control	SO2/WETSCRUB			Sam Şeymour 🧗 🚬 👙 💎 💛 🌣 💮
0.5216	0.2991	no bypass	PM/ESP- CS	2.8976	2.9701	Widows Creek Fossil Plant
-0.0897	0.5557	no bypass	PM/ESP- HS	1.9973	1.9965	Nelson Dewey
-0.096	0.2194	no bypass	PM/ESP- CS	7.4666	6.2152	George Neal South
0	0.3253	no bypass	out of generator	5.3343	3.6393	Wabash River Generating Station
0.3572	-0.1688	no bypass	PM/ESP- CS	16.4719	17.3947	Gibson Generating Station (1099)
0.0495	-2.0104	no bypass	PM/ESP- CS	30.6737	32.3115	Gibson Generating Station (0300)
0.6259	0.6577	no bypass	PM/BAGHOUSE	7.0101	6.6021	Comanche J. (1977)
0.9366	0.952	no bypass	SO2/SDA	1.7035	1.5869	Dwayne Collier Battle Cogeneration Facility
0.0487	-0.1279	no bypass	PM/ESP- CS	4.8266	5.1370	_eland Olds Station
0.3403	-0.3049	no bypass	PM/ESP- HS	10.4083	11.6477	Clifty Creek
-0.2191	0.114	no bypass	PM/PARTSCRUB	3.6996	3.9282	Clay Boswell ****
0.0874	0.0017	no bypass	PM/PARTSCRUB	4.4349	5.6463	Clay Boswell Community (1986)
0.8257	0.8603	no bypass	PM/BAGHOUSE	3.6689	4.0160	Clay Boswell
-0.1742	-0.2317	no bypass	PM/PARTSCRUB	4.3987	4.0213	_awrence
0.3333	0.6574	no bypass	SO2/SDA	5.9733	3.5496	Antelope Valley Station
0.2519	0.3111	no bypass	PM/ESP- CS	4.9119	6.6184	Brayton Point
0.2748	0.2456	no bypass	PM/ESP- CS	4.4348	5.7178	Brayton Point
0.4349	-1.44	no bypass	SO2/SDA	12.5126	13.6164	Wyodak (Fig. 6) The Control of the C
control	coal-stack	location	tested control	furnace	furnace	Plant name
fremove	fr.remove			Hg/TBtu out	lb Hg/TBtu out	_
				F factor lb		

						3 min (1) min
0.9989	0.9992	no bypass	PM/BAGHOUSE	92.5118	43.8616	Scruborass Generating Company L. P.
0.6861	0.7205	no bypass	SO2/WETSCRUB			AES Cayuga (NY) (formerly NYSEG Milliken)
0.7575	0.4567	after bypass	SO2/WETSCRUB			R. D. Morrow Sr. Generating plant
0.4757	0.6513	after bypass	SO2/WETSCRUB			Monticello き こうこう こうしょう こうごう
-0.2126	-0.2037	no bypass	PM/ESP- CS/BAGHOUSE	43.9689	44.0972	Monticello Company of the Company of
0.9975	0.9995	no bypass	PM/BAGHOUSE	32.0152	17.3101	Kline Township Cogen Facility
0.9752	0.9784	no bypass	SO2/SDA	12.0912	11.9526	ogan Generating Plant (19)
0.9736	0.972	no bypass	SO2/SDA	8.6933	8.1477	SEI - Birchwood Power,Facility
control	coal-stack	location	tested control	furnace	furnace	Plant name
fremove	fr.remove			Hg/TBtu out	lb Hg/TBtu out	

			%rel. deviation	F factor lb	% rel deviation F	particulate F factor lb	oxidized F factor lb	elemental F factor lb	inlet last
Plant name	2 F 5 T	lb Hg/TBtu lb	lb Hg/TBtu	Hg/TBtu	factor lb	Hg/TBtu	Hg/TBtu	Hg/TBtu	control
Bruce Mansfield	2.6			7.0985	65%		1.3949	5.5765	141
Craig	0.6	0.6897	2%	0.7248	3%	0.0025	0.0254	0.6969	139
Craig 1000 1000 1000 1000 1000 1000 1000 10		1.3834	9%	1.4456	8%				121
Bailly	2.2	2.2305	11%	2.2306	11%	0.0015	0.2525	1.9766	173
AES Hawaii, Inc.	0.2	0.4452	13%	0.4606	13%	0.0012	0.0149	0.4445	137
Bay Front Plant Generating	6.9	6.9873	197%	3.5792	82%	0.6062	1.6561	1.3169	134
Presque Isle	1.	1.2333	20%	1.2217	16%	0.0208	0.6178	0.5831	153
Présqué Islé	1.	1.2424	8%	1.2622	7%	0.0076	0.5384	0.7162	172
Presque Isle	5.0	5.0896	19%	5.0738	21%	0.0018	0.4267	4.6452	382
TNP-One was the second of the	10.	10.8506	357%	10.8596	338%	0.0414	7.7691	3.0492	181
St Clair Power Plant	3.1	3.1025	58%	3.9076	80%	0.0601	0.9790	2.8685	140
Big Bend	1.8	1.8593	22%	1.5652	20%	0.0000	0.1343	1.4309	155
Navajo	2.7	2.7208	5%	2.7359	3%	0.0214	0.0256	2.6889	155
Valmont	0.1	0.1481	6%	0.1268	4%	0.0042	0.1016	0.0210	147
Intermountain Annual Control of the	2.0	0.2849	11%	0.2466	10%	0.0073	0.0458	0.1935	151
Stockton Cogen Company	2.0	0.2308	4%	0.1316	1%	0.0558	0.0367	0.0391	148
Montrose Andrews Control of the Cont	6.1	6.1366	36%	5.8573	22%	0.0027	1.7884	4.0662	158
Rawhide	7.6	7.6658	52%	7.7630	64%	0.0724	0.5796	7.1110	171
Valley Company of the	1.6	1.8514	21%	1.6630	20%	0.0375	1.3053	0.3203	157
Shawnee Fossil Plant	16	1.0443	7%	1.0507	7%	0.0625	0.4414	0.5468	158
Jim Bridger	4.9	4.9038	37%	4.7040	35%	0.0340	0.1780	4.4920	146
Laramie River Station	2.6	2.6154	42%	3.0184	49%				138
Laramie River Station	3.0	3.0504	34%	3.3411	58%	-0.0133	-0.2722	3.6265	139
La Cygne	5.C	5.0527	105%	5.5140	132%	0.1217	0.3073	5.0850	144
Cliffside Advantage Communication Communicat	4.9	4.9826	110%	4.3223	108%	0.1433	2.1641	2.0149	342
Sherburne County Generating Plant	7.1	7.1935	92%	7.5401	132%	0.1276	0.1455	7.2670	147
Meramec () () () () () () ()	1.9	1.9267	74%	1.7255	64%	0.0031	1.0719	0.6505	170
Colstrip	5.1	5.1853	306%	5.7264	341%	0.0873	0.3028	5.3363	139
GRDA AND AND AND AND AND AND AND AND AND A	8.3	8.3264	114%	8.6918	60%	0.0117	0.7602	7.9199	156
Coronado Servicio de Contracto	2.1	2.1357	22%	2.4468	13%	0.0509	0.0508	2.3451	138
Newton	7.6	7.6305	81%	6.9877	59%	0.0024	1.4250	5.5603	161
Salem Harbor	0.3	0.3291	14%	0.3348	16%	0.0589	0.0997	0.1762	126
Columbia	10.	10.2732	23%	10.3097	25%	0.0034	1.8045	8.5018	406
Cholla	1.0	1.0763	47%	1.2066	50%	0.0000	0.2139	0.9927	359
Cholla	2.6	2.6906	22%	3.1864	25%	0.0000	0.1173	3.0691	137
Platte	****** 11.	1.4905	305%	10.6121	286%	0.0182	0.8939	9.7000	414

		%r <u>A</u>		0% rel	nariculate	- DAZIDIZA	elemental	
		deviation	F factor lb	deviation F	F factor lb	factor lb	F factor lb	inlet last
	lb Hg∕TBtu	lb Hg/TBtu	Hg/TBtu	factor lb	Hg/TBtu	Hg/TBtu	Hg/TBtu	control
Plant name	out control	out control	out control	Hg/TBtu	out control	out control	out control	temp (C)
Wyodak	8.0526	6%	7.0701	3%	0.0136	0.1152	6.9413	160
Brayton Point	3.3877	31%	3.2000	30%	0.5478	2.4042	0.2479	154
Brayton Point And	3.8926	93%	3.6979	101%	0.4019	2.1687	1.1273	122
Antelope Valley Station	2.0791	169%	4.0042	324%	0.0128	0.3236	3.6678	153
Lawrence	4.755	10%	5.1181	21%	0.1349	0.3660	4.6172	166
Clay Boswell Clay	0.6863	39%	0.6633	34%	0.0204	0.5271	0.1158	176
Clay Boswell	5.147	10%	4.0454	15%	0.0013	0.0412	4.0029	144
Clay Boswell	4.8364	24%	4.4550	35%	0.1176	0.2688	4.0686	144
Cliffy Creek	8.3071	40%	6.8745	53%	0.1853	3.3834	3.3058	383
Leland Olds Station	4.0512	136%	4.0233	76%	0.0017	0.6844	3.3372	202
Dwayne Collier Battle Cogeneration Facility	0.1037	1%	0.1074	1%	0.0225	0.0190	0.0659	168
Comanche . 32	2.6611	45%	2.5931	42%	0.0194	2.3172	0.2565	145
Gibson Generating Station (0300)	30.7445	324%	29.0614	205%	0.0069	24.9348	4.1197	156
Gibson Generating Station (1099)	12.9877	405%	9.7452	164%	0.0228	6.1032	3.6192	161
Wabash River Generating Station	3.6393	32%	5.3343	37%	0.0477	0.5454	4.7412	176
George Neal South	5.7757	66%	7.7269	75%	0.0303	3.2082	4.4883	152
Nelson Dewey	2.0488	34%	2.1349	41%	0.0207	0.1603	1.9539	257
Widows Creek Fossil Plant	1.3695	32%	1.3986	37%	0.0649	0.8161	0.5176	160
Sam Seymour Control of the Second Control of	4.4806	49%	8.6353	49%	0.0498	0.1957	8.3898	150
Polk Power	5.2289	37%	5.4713	31%	0.0071	0.3951	5.0691	171
R.M. Heskett Station	3.5095	52%	3.9768	44%	0.0552	0.4895	3.4321	162
Stanton Station	3.9569	27%	6.9024	17%	0.0136	0.2496	6.6392	165
Stanton Station Station	8.1445	15%	6.2517	15%	0.0044	0.1361	6.1112	176
Charles R. Lowman	1.001	229%	0.9706	221%				146
Dunkirk and the second of the	8.3976	195%	6.8030	145%	0.1502	4.2746	2.3782	305
Jack Watson 2017年10年10年10日 10日 10日 10日 10日 10日 10日 10日 10日 10日	3.0657	49%	2.9333	24%	0.0256	2.0258	0.8819	150
San Juan September 1985	4.0847	110%	4.2854	104%	0.0447	0.2712	3.9695	143
Mecklenburg Cogeneration Facility	0.1029	2%	0.1062	2%	0.0105	0.0418	0.0539	148
Port Washington	6.359	31%	6.6916	27%	0.0110	4.4920	2.1886	406
Lewis & Clark	9.1641	99%	10.8315	76%	0.0164	0.3229	10.4922	199
Clover Power Station	0.3387	20%	0.3529	21%	0.0239	0.1914	0.1376	139
W. H. Sammis	1.0109	6%	0.8291	3%	0.0368	0.3808	0.4115	158
Big Brown	29.3912	97%	30.0889	91%	0.0413	12.6207	17.4269	185
Gaston	6.1698	104%	6.0738	75%	0.5508	3.6455	1.8775	336
Coyote	7.355	628%	7.9523	677%	0.0733	0.1686	7.7105	172
Limestone	13.8843	85%	13.6612	46%	0.1194	1.7118	11.8300	162

Scrubgrass Generating Company L. P.	AES Cayuga (NY) (formerly NYSEG Milliken)	R. D. Morrow Sr. Generating plant	Monticello	Monticello	Kline Township Cogen Facility	Logan Generating Plant	SEI - Birchwood Power Facility				
0.0485	2.1612	2.0909	16.7222	56.0352	0.0326	0.2728	0.2444	out control	lb Hg/TBtu		
0.3%	15%	22%	249%	2779%	0.1%	27%	15%	out control out control out control	lb Hg/TBtu lb Hg/TBtu Hg/TBtu	deviation	%rel.
0.0936	2.0652	2,1269	18.3232	55.8686	0.0816	0.2801	0.2379	out control	Hg/TBtu	F factor lb	
1%	13%	19%	511%	2770%	0.3%	27%	15%	Hg∕TBtu	factor lb	deviation F	% rel
0.0020	0.0091			0.0922	0.0025	0.0127	0.0092	out control	Hg/TBtu	F factor lb	힜
0.0367	0.1465			47.4770	0.0308	0.0270	0.1223	out control out control out control	Hg/TBtu	factor lb	articulate oxidized F elementa
0.0550	1.9096			8.2994	0.0484	0.2403	0.1064	out control	Hg/TBtu	F factor lb	elemental
161	137	166	176	181	188	147	134	temp (C)	control	inlet last	

	stack temp	ы Нд∕ТWН	from	lb Hg/MWH	from
Plant name	(C)		concentration	from coal	concentration
Bruce Mansfield	52.3	66.34	75.24	0.00006634	0.00007524
Craig (1971)	81.9	7.31	7.68	0.00000731	0.00000768
Craig	62.0	14.66	15.32	0.00001466	0.00001532
Bailly	54.2	23.64	23.64	0.00002364	0.00002364
AES Hawaii, Inc.	133.5	4.72	4.88	0.00000472	0.00000488
Bay Front Plant Generating	133.7	74.07	37.94	0.00007407	0.00003794
Presque Isle	151.7	13.07	12.95	0.00001307	0.00001295
Presque Isle	171.9	13.17	13.38	0.00001317	0.00001338
Presque Isle	195.7	53.95	53.78	0.00005395	0.00005378
TNP-One	175.3	115.02	115.11	0.00011502	0.00011511
St Clair Power Plant	140.0	32.89	41.42	0.00003289	0.00004142
Big Bend	52.0	19.71	16.59	0.00001971	0.00001659
Navajo (2000)	49.0	28.84	29.00	0.00002884	0.00002900
Valmont	140.0	1.57	1.34	0.00000157	0.00000134
Intermountain (1)	48.7	3.02	2.61	0.00000302	0.00000261
Stockton Cogen Company	146.0	2.45	1.39	0.00000245	0.00000139
Montrose 12 12 12 12 12 12 12 12 12 12 12 12 12	167.2	65.05	62.09	0.00006505	
Rawhide Communication of the C	104.0	81.26	82.29	0.00008126	0.00008229
Valley Andrew Control of the Control	158.4	19.62	17.63	0.00001962	0.00001763
Shawnee Fossil Plant	151.3	11.07	11.14	0.00001107	0.00001114
Jim Bridger AND	53.7	51.98	49.86	0.00005198	0.00004986
Laramie River Station	63.7	27.72	32.00	0.00002772	
Laramie River Station	78.5	32.33	35.42	0.00003233	
La Cygne	72.7	53.56	58.45	0.00005356	
Cliffside TOTA TOTAL TOT	194.5	52.82	45.82	0.00005282	0.00004582
Sherburne County Generating Plant	80.3	76.25	79.93	0.00007625	0.00007993
Meramec	158.3	20.42	18.29	0.00002042	0.00001829
Colstrip	89.0	54.96	60.70	0.00005496	0.00006070
GRDA CARLOS CONTROL OF THE CONTROL O	84.1	88.26	92.13	0.00008826	
Coronado	48.0	22.64	25.94	0.00002264	
Newton 10 10 10 10 10 10 10 10 10 10 10 10 10	167.3	80.88	74.07	0.00008088	0.00007407
Salem Harbor	128.7	3.49	3.55	0.00000349	0.00000355
Columbia	154.0	108.90	109.28	0.00010890	
Cholla	157.7	11.41	12.79	0.00001141	
Cholla	86.7	28.52	33.78	0.00002852	
Platte	154.8	121.80	112.49	0.00012180	0.00011249

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-Imestone	Coyote	Gaston	Big Brown	W. H. Sammis	Clover Power Station	ewis & Clark	Port Washington	Mecklenburg Cogeneration Facility	San Juan	Jack Watson	Dunkirk Company of the Company of th	Charles R. Lowman	Stanton Station	Stanton Station	R.M. Heskett Station	Polk Power	Sam Seymour	Widows Creek Fossil Plant	Nelson Dewey	George Neal South	Wabash River Generating Station	Gibson Generating Station (1099)	Gibson Generating Station (0300)	Comanche	Dwayne Collier Battle Cogeneration Facility	eland Olds Station	Cliffy Creek	Clay Boswell	Clay Boswell	Tay Down I Company of the Company of	Antelope Valley Station	Brayton Point	Brayton Point	Wyodak	Plant name		
がら かんかん あいまま												,													cility								, .				
59.7	102.3	126.7	167.3	150.7	50.2	60.0	205.9	74.6	47.9	152.3	294.8	122.0	93.3	166.5	157.7		55.7	157.0	260.0	141.3		171.7	155.0	151.5	85.7	182.0	167.3	68.0	510	67.3	84.0	124.7	143.0	81.7	<u>(C</u>	stack temp	
147.17	77.96	65.40	311.55	10.72	3.59	97.14	67.41	1.09	43.30	32.50	89.01	10.61	86.33	41.94	37.20	55.43	47.49	14.52	21.72	61.22	38.58	137.67	325.89	28.21	1.10	42.94	88.06	51.27	7.27	50.40	22.04	41.26	35.91	85.36	from coal	b Hg/TWH	
144.81	84.29	64.38	318.94	8.79	3.74	114.81	70.93	1.13	45.43	31.09	72.11	10.29	66.27	73.17	42.15	58.00	91.53	14.83	22.63	81.91	56.54	103.30	308.05	27.49	1.14	42.65	72.87	47.22	7.03	54.25	42.44	39.20	33.92	74.94	concentration	from	lb Hg/TWH
0.00014717	0.00007796	0.00006540	0.00031155	0.00001072	0.00000359	0.00009714	0.00006741	0.00000109	0.00004330	0.00003250	0.00008901	0.00001061	0.00008633	0.00004194	0.00003720	0.00005543	0.00004749	0.00001452	0.00002172	0.00006122	0.00003858	0.00013767	0.00032589	0.00002821	0.00000110	0.00004294	0.00008806	0.00005127	0.00000727	0.00005040	0.00002204	0.00004126	0.00003591	0.00008536	from coal	lb Hg/MWH	
0.00014481	0.00008429	0.00006438	0.00031894	0.00000879	0.00000374	0.00011481	0.00007093	0.00000113	0.00004543	0.00003109	0.00007211	0.00001029	0.00006627	0.00007317	0.00004215	0.00005800	0.00009153	0.00001483	0.00002263	0.00008191	0.00005654	0.00010330	0.00030805	0.00002749	0.00000114	0.00004265	0.00007287	0.00004288	0.00000703	0.00005425	0.00004244	0.00003920	0.00003392	0.00007494	concentration	from	HWM/pH dl

	1	45 	AES Cayuga (NY) (formerly NYSEG Milliken)	R. D. Morrow Sr. Generating plant	Monticello (1977) The state of	Monticello		Logan Generating Plant	SEI - Birchwood Power Facility	Plant name	st		
		157.0	50.1	86.3	89.3	165.3	173.7	87.0	90.0	0	tack temp		
* the value o 0.322115 for		0.51	22.91	22.16	177.26	593.97	0.35	2.89	2.59	from coal	stack temp lb Hg/TWH		
* the value of MWH was estimated with 0.322115 for power conversion.		0.99	21.89	22.55	194.23	592.21	0.86	2.97	2.52	concentration	from	lb Hg/TWH	
ted with		0.00000051	0.00002291	0.00002216	0.00017726	0.00059397	0.00000035	0.00000289	0.00000259	from coal	lb Hg/MWH		
an efficiency of		0.00000099	0.00002189	0.00002255	0.00019423	0.00059221	0.00000086	0.00000297	0.00000259 0.00000252	concentration	from	lb Hg/MWH	

You may search these terms through the use of the find or [Ctrl][f] keys.

The monthly mercury tests by coal type are reported for all units at the facility. The unit tested at the facility may burn one or more of the types of coal types that were tested for mercury. You should manually match the type of fuel during the emissions test to the types of coals measured during the year for comparison purposes.

NOTES FOR CALCULATIONS

Some FGD units were operated with an active bypass of the control device during the testing. For units with a bypass around the unit (some of the furnace gas was vented to the stack without treatment by the control device) the measured data were used to estimate the concentration and flow rates as if all of the gas were treated by the control device.

For units with multiple control devices in series, only the last control device was tested. Those units with multiple controls in series had no direct measurements of the furnace exit gas before the first control, and **those** calculations of the exiting furnace gas are reported as zero in the detail data and are blank in the summary data.

Mercury concentrations that are reported as non-detect are estimated as one half the quantification limit.

In a few cases the fraction removed is negative. These negative numbers are reported as calculated on the same basis as the other numbers, without setting the fraction to zero removal. A removal that is less than zero is a physical impossibility and should be viewed as an artifact of the test program.

The mercury loading factors (lb Hg/TBtu) are calculated by two methods, (1) the mercury rate divided by the heating rate of the coal and (2) the concentration of Hg multiplied by an F factor and corrected for oxygen content. The F factor method is thought to be more accurate because of potential problems in reporting coal feed rates and flue gas flow rates.

The two methods for evaluating the mercury loading factors (lb Hg/TBtu) may produce significantly different results. When this difference occurs, the reason is often due to test report inaccuracies of the flow rates of the gas entering the control device. In the case of Montrose, the flow rate into the control device was reported as one fourth of the total flow rate of gas, and the loading based upon this lower flow gas flow rate was also one fourth of the loading based upon concentration (F factor). Possibly three fourths of the flow was diverted to other control units.

In some of the units (Valmont, Craig Unit 3), the mercury concentrations reported for the coal analysis were less than the mercury concentrations reported during the yearly tests. In the case of Valmont, the mass balances of the mercury out of the furnace would have been better if the typical or yearly average values were used. In the case of Craig Unit 3 the mass balances are better with the reported test mercury concentrations in the coal. The reported concentrations for the test data are used for the calculations, with the possible exception of Polk (see the comment for Polk under detail data).

Speciation values were obtained for the runs that reported Hg measured as particulate, oxidized, and elemental directly downstream of the tested unit. In these cases, the fraction of Hg in the speciation was calculated as the average value of the species for the three runs, divided by the average value of the sum of all species for the three runs. The lb Hg/TBtu for each species was the product of the value for the lb total Hg/TBtu and the fraction of Hg for the species.

Speciation values were reported for Hg downstream of the tested unit. In some cases, the speciation values were measured after the return and mixing of gas that bypassed the control device. Estimation of the speciation values by material balance is believed to be in error and is not reported in the data set. Negative values for the particulate and oxidized Hg were calculated and are thought to be in error due to measurement artifacts upstream of the control device or speciation rearrangement during the bypass duct flow.

COAL TESTING TERMS

MONTH = The month of the testing, 1 is January, 2 is Feb., etc.

number measurements = The number of mercury concentrations reported for the month.

number nondetects = The number of mercury concentrations reported that were below the quantitation limit.

average Hg in fuel (ppmw) = The monthly average for the fuel type, parts per million by weight.

percent relative deviation (PRD) = The ratio of the standard deviation to the average, expressed as a percentage

standard deviation (ppmw) = The standard deviation of the monthly mercury concentrations.

highest (ppmw) = The greatest value of the mercury content reported for the month.

lowest (ppmw) = The least value of the mercury content reported for the month.

MISCELLANEOUS TERMS	
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Tested control = The name of the tested mercury control device(s).

LOCATION = The position of the exit sample port with respect to the bypass vent where one exists. After control means that the control exit was sampled before the return of the bypass gas. After bypass means that the control exit was sampled after the return of the bypass gas.

name of fuel = In the column heading, this term refers to the fuel type that was tested on a monthly basis.

fuel in test = The fuel type that was burned during the emissions test.

SPECIATION = Refers to the type of mercury that is present: as elemental, as oxidized, or as sorbed on particulate matter.

ELEMENTAL MERCURY = Mercury that is present in the elemental or unoxidized form in the duct or stack gas stream.

OXIDIZED MERCURY = Mercury that is present in a compound form with chlorine, oxygen, or other oxidants in the duct or stack gas stream.

PARTICULATE MERCURY= Mercury that is sorbed on the particulate matter in the duct or the stack gas stream.

UNIT NAME = Most facilities have multiple units. This is the assigned name for the unit that was tested.

average Hg in fuel (ppmw) = The average mercury concentration measured in the fuel (from 1999 year testing).

CI in test coal (ppmw) = The average chlorine for the coal during the emissions test.

Hg in test coal (ppmw) = The average mercury for the coal during the emissions test.

Hg out furnace/ Hg in coal = The ratio of the mercury in the exiting furnace gas to the mercury in the coal. This number is expected to equal approximately one.

Ib Hg/TBtu out furnace = The pounds of mercury leaving the furnace per trillion Btu in the coal. Estimated from the measured concentrations and flow rates of coal and gas.

F factor lb Hg/TBtu out furnace = The exit concentration in the furnace gas multiplied by a conversion Fuel Factor (F) and corrected for the oxygen concentration in the gas. The Fuel Factor was 9840 dscf/10⁶ Btu. The oxygen correction was 20.9/(20.9-O), where O is the percent oxygen in the combustion gas.

fr.remove coal-stack = The fraction of the mercury in the coal that is removed before exiting the stack. This estimate assumes that all of the gas is treated by the control device. (corrected for bypass)

fremove control = The fraction of the mercury in the treated gas that is removed by the control device that was tested.

Ib Hg/TBtu out control = The pounds of mercury leaving the control per trillion Btu in the coal. Estimated from the measured concentrations and flow rates of coal and gas.

F factor lb Hg/TBtu out control = The exit Hg concentration from the control device multiplied by a conversion fuel factor (F) and corrected for the oxygen concentration in the gas.

particulate F factor Ib Hg/TBtu out control = The concentration of Hg sorbed on particulate that is measured exiting the control device multiplied by a conversion fuel factor (F) and corrected for the oxygen concentration in the gas.

oxidized F factor lb Hg/TBtu out control = The concentration of oxidized Hg that is measured exiting from the control device multiplied by a conversion fuel factor (F) and corrected for the oxygen concentration in the gas.

elemental F factor lb Hg/TBtu out control = The concentration of elemental Hg that is measured exiting from the control device multiplied by a conversion fuel factor (F) and corrected for the oxygen concentration in the gas.

Inlet last control temp (C) = The temperature in Celsius of the gas entering the control device.

stack temp (C) = The temperature in Celsius of the gas exiting the control device. In most cases this is measured in the stack.

Ib Hg/TWH from coal = The Hg emissions (lb Hg) per electric power generation rate (TWH, tera watt hour) from the coal. The fuel rate and heat content is used for the energy rate from coal combustion. Assumes a power conversion efficiency of 0.322. Ib Hg/TWH is one million times greater than lb Hg/MWH.

Ib Hg/TWH from concentration = The Hg emissions (lb Hg) per electric power generation rate (TWH, tera watt hour) from the coal. The oxygen concentration is used to estimate the energy rate using the F factor. Assumes a power conversion efficiency of 0.322.

Ib Hg/MWH from coal = The Hg emissions (lb Hg) per electric power generation rate (MWH, mega watt hour) from the coal. The fuel rate and heat content is used for the energy rate from coal combustion. Assumes a power conversion efficiency of 0.322.

Ib Hg/MWH from concentration = The Hg emissions (lb Hg) per electric power generation rate (MWH, mega watt hour) from the coal. The oxygen concentration is used to estimate the energy rate using the F factor. Assumes an energy efficiency conversion to electricity of 0.322.

EMISSION MODIFICATION FACTOR = A fraction with a range of 1.0 - 0.0 that represents the ratio of the mercury discharged from a control device to the mercury present in the control device entrance. If a control device has little effect on the mercury removal, the emission modification factor will be approximately 1.0. If the control device removes 90% of the mercury, the emission modification factor will be 0.1.

EMF = Abbreviation for Emission Modification Factor

PERCENT REMOVAL = the percent of the mercury that is removed by the control device. In general, the percent removal is presented as one number that represents the combined effect of the fuel, the boiler type, the NO_X control, the particulate control, and the SO_X control.

FURNACE/BOILER = Terms used to describe the combustion device used to convert coal into carbon dioxide and water with the chemical release of heat used to create steam for power generation. The furnace combusts fuel; the boiler converts water to steam.

 SO_x = Oxides of sulfur. These include precursors of sulfuric acid, formed by reaction with water in the atmosphere.

 NO_X = Oxides of nitrogen. These include precursors of nitric acid, formed by reaction with water in the atmosphere.

PM = Particulate material. Coal contains some minerals that are not consumed in the combustion process, but remain as ash or particulate material potentially discharged in the stack gas.

FUEL TYPE

ANTHRACITE = Anthracite coal is a combustible rock composed of organic and mineral materials that has formed over time by vegetative decay and mineral deposition. The properties of coal vary depending on the type of vegetative matter and the formation conditions (reference ASTM D 388-82). In general, anthracite coal has a higher heating content (Btu/lb) than bituminous coal.

BITUMINOUS = Bituminous coal is a combustible rock composed of organic and mineral materials that has formed over time by vegetative decay and mineral deposition. The properties of coal vary depending on the type of vegetative matter and the formation conditions (reference ASTM D 388-82). Bituminous Coal has a higher heating content (Btu/lb) than Subbituminous coal.

BITUMINOUS - HIGH SULFUR = Assumed to be a bituminous coal. This extra nomenclature was sought by certain units participating in the 1999 Electric Utility Steam Generating Unit Mercury Emissions Information Collection Effort (EU/ICE) in order to keep their higher and lower sulfur fuels separate.

BITUMINOUS - LOW SULFUR = Assumed to be a bituminous coal. This extra nomenclature was sought by certain units participating in the 1999 EU/ICE in order to keep their higher and lower sulfur fuels separate.

SUBBITUMINOUS = Subbituminous coal is a combustible rock composed of organic and mineral materials that has formed over time by vegetative decay and mineral deposition. The properties of coal vary depending on the type of vegetative matter and the formation conditions (reference ASTM D 388-82). Subbituminous coal has a higher heating content (Btu/lb) than lignite coal.

LIGNITE = Lignite coal is a combustible rock composed of organic and mineral materials that has formed over time by vegetative decay and mineral deposition. The properties of coal vary depending on the type of vegetative matter and the formation conditions (reference ASTM D 388-82). Lignite coal has the lowest higher heating content (Btu/lb) of the four major coal rankings.

PETROLEUM COKE = Petroleum coke (also called petcoke) is a carbonaceous by-product of the petroleum refining process and is burned as a supplemental fuel with coal.

WASTE BITUMINOUS = Waste bituminous coal reclaimed from mine waste piles.

WASTE SUBBITUMINOUS = Waste subbituminous coal reclaimed from mine waste piles.

WASTE ANTHRACITE = Waste anthracite coal reclaimed from mine waste piles.

TIRES = Tire derived fuel (TDF), that refers to the use of scrap tires as a substitute for a fossil fuel. As with petroleum coke it is burned as a supplemental fuel with coal.

FURNACE TYPE_

CONV/PC = Conventional, pulverized coal-firing furnace. In pulverized-coal-fired boiler systems, coal is pulverized in a mill to the consistency of talcum powder (i.e., at least 70 percent of the particles will pass through a 200-mesh sieve). The pulverized coal is generally entrained in primary air before being fed through the burners to the combustion chamber, where it is fired in suspension.

FBC = Fluidized-bed combustor. In an FBC, combustion occurs when coal, together with inert material (e.g., sand, silica, alumina, or ash) and/or a sorbent such as limestone, are suspended through the action of primary combustion air distributed below the combustor floor. "Fluidized" refers to the state of the bed of material (fuel or fuel and inert material [or sorbent]) as gas passes through the bed.

COAL GAS = Integrated Coal Gasification Combined Cycle Units. At a coal gasification power plant the coal-fired boiler unit is replaced with a coal gasification unit coupled with a gas turbine combustor and heat recovery boiler. The solid coal is gasified by a process in which a coal/water slurry is reacted at high temperature and pressure with oxygen (or air) and steam in a vessel (the gasifier) to produce a combustible gas. This combustible gas is composed of a mixture of carbon dioxide and hydrogen and is often referred to as a synthetic gas or syngas.

CYCLONE = Cyclone firing uses several water-cooled horizontal burners that produce high-temperature flames that circulate in a cyclonic pattern. The burner design and placement cause the ash to become a molten slag that is collected below the furnace.

STOKER = Stoker-fired furnace. In stoker furnaces, coal is burned on a bed at the bottom of the furnace. The bed of coal burns on a grate. Heated air passes upward through openings in the grate.

TURBO = Turbo-fired. This furnace is a specialized form of a conventional coal-fired furnace.

WET or DRY = Furnaces are classified as either dry or wet bottom, depending on the ash removal technique. Dry bottom furnaces fire coals with high ash fusion temperatures, and dry ash removal techniques are used. In wet bottom (slag tap) furnaces, coal with a low ash fusion temperature is used, and molten ash is drained from the bottom of the furnace.

NO.	control technology_		

 NO_X = Combustion NO_X controls. A variety of combustion control practices can be used including low NO_X burners, overfire air, off-stoichiometric firing, selective or biased burner firing, reburning, and burners-out-of- service. Control of NO_X can also be achieved through staged combustion (also called air staging).

 $NONOX = No combustion NO_X controls on the furnace.$

SCR = Selective Catalytic Reduction (a post combustion, add-on, NO_X control device). The selective catalytic reduction (SCR) process uses a catalyst with ammonia gas (NH3) to reduce the NO and NO₂ in the flue gas to molecular nitrogen and water.

SNCR = Selective Noncatalytic Reduction (a post combustion, add-on, NO_X control device). The selective noncatalytic reduction (SNCR) process is based on the same basic chemistry of reducing the NO and NO_2 in the flue gas to molecular nitrogen and water as the SCR but does not require the use of a catalyst to prompt these reactions.

Sulfur Dioxide control technology_

WETSCRUB = A flue gas desulfurization wet scrubber (FGD, [lime or limestone]), in which flue gas containing SO_2 is brought into contact with a limestone-water slurry. The SO_2 is absorbed into the slurry and reacts with limestone to form an insoluble sludge.

COMP COAL = Compliance coal has a specifically desired low sulfur content to bring emissions into compliance with SO_2 regulations. Compliance coal may be obtained through the mining of lower-sulfur coals, coal washing, and/or coal blending.

SDA = Dry lime/spray dryer adsorber followed by a baghouse. In an SDA, flue gas is contacted with fine spray droplets of hydrated lime slurry in a spray dryer vessel. The SO₂

is absorbed in the slurry and reacts with the hydrated lime reagent to form solid calcium sulfite and calcium sulfate as in a wet lime scrubber. The water is evaporated by the heat of the flue gas. The dried solids are entrained in the flue gas, along with fly ash, and are collected in a baghouse.

SDAESP = Dry lime/spray dryer adsorber followed by a cold-side ESP.

FBC = In an SO₂ control context, FBC refers to the use of a sorbent such as limestone in the furnace's fluidized bed for SO₂ control.

SORBENT INJ = Dry injection process, dry powdered lime (or another suitable sorbent) is directly injected into the ductwork upstream of a PM control device.

SORBESP = A dry injection process (mentioned above) located before a cold-side ESP.

Particulate matter control technology_

ESP- CS = Electrostatic precipitator (cold-side, meaning this ESP is installed at a location downstream of the air preheater). The ESP operates by imparting an electrical charge to incoming particles, then attracting the particles to oppositely charged plates for collection. The collected particles are periodically dislodged in sheets or agglomerates by rapping or otherwise vibrating the plates.

BAGHOUSE = Baghouse (fabric filter) that collects PM by placing a fabric barrier in the flue gas path. Gas passes freely through the fabric, but particles are trapped and retained for periodic removal.

MECH/BAGHOUSE = A mechanical collector followed by a fabric filter.

ESP- HS = Electrostatic precipitator (hot-side, meaning this ESP is installed at a location upstream of the air preheater). Operates by imparting an electrical charge to incoming particles, then attracting the particles to oppositely charged plates for collection. The collected particles are periodically dislodged in sheets or agglomerates by rapping or otherwise vibrating the plates.

ESP- CS/BAGHOUSE = A cold-side ESP followed by a fabric filter.

MECH = Mechanical collector (assumed to be a cyclone collector in this database). Flue gas entering a cylinder tangentially to the wall is imparted with a circular motion around the cylinder's axis. Particles in the gas stream are forced toward the wall by centrifugal force, then downward through a conical discharge at the bottom of the cylinder.

MECH/ESP- CS = A mechanical collector followed by a cold-side ESP.

PARTSCRUB = Particulate scrubber. Particulate scrubbers operate by shattering streams of water into small droplets that collide with and trap solid particles contained in the flue gas or by forcing the gases into intimate contact with water films. The particle-laden droplets or water films coalesce and are collected in a sump at the bottom of the scrubber.

PARTSCRUB/ESP- CS = A cold-side ESP followed by a particulate scrubber.

MECH/PARTSCRUB = A mechanical collector followed by a particulate scrubber.

MECH/BAGHOUSE/ESP- HS = A mechanical collector followed by a hot-side ESP followed by a fabric filter.

ESP- HS/ESP- CS = A hot-side ESP followed by a cold-side ESP.

ESP- HS/BAGHOUSE = A hot-side ESP followed by a fabric filter.

ESP- CS/ESP- CS = Two cold-side ESPs in series. The first cold-side ESP is less efficient and requires a particle polisher for the second, more efficient cold-side ESP.